

Elastic constants

2nd rank tensor

Hooke's Law $\sigma_{ij} = \sum_{kl} C_{ijkl} \varepsilon_{kl}$ only 36 components required due to symmetries in σ_{ij} and ε_{kl}

4th order tensor

Using the Voigt notation for a symmetric tensors,
to re-write Hooke's Law in matrix-times-vector form

1=xx, 2=yy, 3=zz, 4=yz, 5=zx, 6=xy

		compression		mixed		
$\begin{pmatrix} \sigma_{xx} \\ \sigma_{yy} \\ \sigma_{zz} \\ \sigma_{yz} \\ \sigma_{zx} \\ \sigma_{xy} \end{pmatrix}$	=	$\begin{pmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{pmatrix}$	$\begin{pmatrix} C_{14} & C_{15} & C_{16} \\ C_{24} & C_{25} & C_{26} \\ C_{34} & C_{35} & C_{36} \end{pmatrix}$	$\begin{pmatrix} \varepsilon_{xx} \\ \varepsilon_{yy} \\ \varepsilon_{zz} \\ \varepsilon_{yz} \\ \varepsilon_{zx} \\ \varepsilon_{xy} \end{pmatrix}$		
stress		mixed	shear	strain	compression	shear

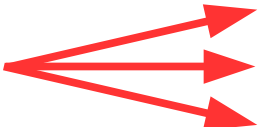
Considering the possibility to exchange indexes $C_{12} = C_{21}$
there are 21 independent elastic constants

Elastic constants with cubic symmetry

Cubic symmetry: only 3 independent elastic constants C_{11} , C_{12} , C_{44}

$$\begin{pmatrix} C_{11} & C_{12} & C_{12} & 0 & 0 & 0 \\ C_{12} & C_{11} & C_{12} & 0 & 0 & 0 \\ C_{12} & C_{12} & C_{11} & 0 & 0 & 0 \\ 0 & 0 & 0 & C_{44} & 0 & 0 \\ 0 & 0 & 0 & 0 & C_{44} & 0 \\ 0 & 0 & 0 & 0 & 0 & C_{44} \end{pmatrix}.$$

Transformation due to the strain

Lattice vectors of the unit cell  $\begin{pmatrix} \mathbf{a}_1 \\ \mathbf{a}_2 \\ \mathbf{a}_3 \end{pmatrix} = \begin{pmatrix} a_{1x} & a_{1y} & a_{1z} \\ a_{2x} & a_{2y} & a_{2z} \\ a_{3x} & a_{3y} & a_{3z} \end{pmatrix}$

Transformation of the lattice vectors due to the strain:

$$\begin{pmatrix} \mathbf{a}'_1 \\ \mathbf{a}'_2 \\ \mathbf{a}'_3 \end{pmatrix} = \begin{pmatrix} \mathbf{a}_1 \\ \mathbf{a}_2 \\ \mathbf{a}_3 \end{pmatrix} (\hat{I} + \hat{\varepsilon})$$

where

$$\hat{I} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \quad \hat{\varepsilon} = \begin{pmatrix} e_1 & e_6/2 & e_5/2 \\ e_6/2 & e_2 & e_4/2 \\ e_5/2 & e_4/2 & e_3 \end{pmatrix} \quad \text{- strain tensor}$$

Total energy of the distorted lattice

$$E = E_0 - P(V_0)\Delta V + \frac{1}{2}V_0 \sum_{i=1}^6 \sum_{j=1}^6 C_{ij}e_i e_j$$

E_0 - total energy of the undistorted lattice

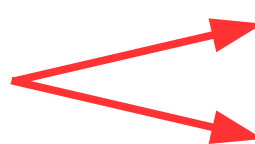
V_0 - volume of the undistorted lattice

$P(V_0)$ - pressure of the undistorted lattice at volume V_0

ΔV - change of the volume due to the strain

C_{ij} - elastic constants of the lattice (21 independent due to symmetry)

e_i - elements of the strain tensor

Strain  volume conserving $\Delta V = 0$
not volume conserving $\Delta V \neq 0$

Total energy of the distorted lattice

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Strain

volume conserving $\Delta V = 0$

not volume conserving $\Delta V \neq 0$

in this lab

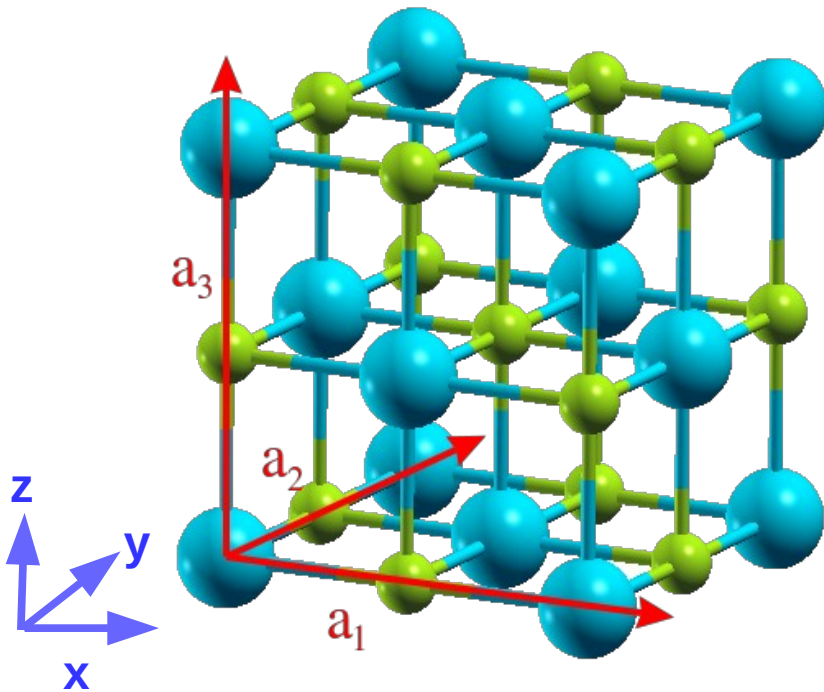
Strain of the system with a cubic symmetry

Cubic symmetry



Only 3 independent elastic constants: C_{11}, C_{12}, C_{44}

$$B = \frac{1}{3} (C_{11} + 2C_{12}) \text{ - bulk modulus}$$



$$\begin{pmatrix} \mathbf{a}_1 \\ \mathbf{a}_2 \\ \mathbf{a}_3 \end{pmatrix} = \begin{pmatrix} a_0 & 0 & 0 \\ 0 & a_0 & 0 \\ 0 & 0 & a_0 \end{pmatrix}$$

a_0 - equilibrium lattice parameter

Determine the positions of 8 inequivalent C atoms in the *conventional* unit cell of diamond on the figure above and specify them in your input file. Remember to change the parameter `nat`.

Determination of the elastic constants C_{11} and C_{12}

Tetragonal strain:

$$\hat{\varepsilon} = \begin{pmatrix} x & 0 & 0 \\ 0 & -x & 0 \\ 0 & 0 & \frac{x^2}{1-x^2} \end{pmatrix}$$

x - unitless parameter

Determine the change of the lattice parameters due to such a strain:

$$\begin{pmatrix} \mathbf{a}'_1 \\ \mathbf{a}'_2 \\ \mathbf{a}'_3 \end{pmatrix} = \begin{pmatrix} \mathbf{a}_1 \\ \mathbf{a}_2 \\ \mathbf{a}_3 \end{pmatrix} (\hat{I} + \hat{\varepsilon}) = \dots$$

Change of the total energy due to such a strain:

$$\Delta E(x) = \Delta E(-x) = V_0(C_{11} - C_{12})x^2$$

Make a fit with this function, and use the expression for the bulk modulus in order to determine C_{11} , C_{12}

POINT [A]

Use the [orthorhombic unit cell](#) in order to model such a strain:

$$\text{ibrav} = 8$$

$$\text{celldm}(1) = |\mathbf{a}'_1|$$

$$\text{celldm}(2) = |\mathbf{a}'_2|/|\mathbf{a}'_1|$$

$$\text{celldm}(3) = |\mathbf{a}'_3|/|\mathbf{a}'_1|$$

POINT [B]

Set up the system using $\text{ibrav} = 0$ and the `CELL_PARAMETERS` card as described online in the input manual.

Can you get the same results?

Relax your structure for every value of x , in order to find the minimum of energy!

Determination of the elastic constant C_{44}

$$\hat{\varepsilon} = \begin{pmatrix} 0 & \frac{x}{2} & 0 \\ \frac{x}{2} & 0 & 0 \\ 0 & 0 & \frac{x^2}{4-x^2} \end{pmatrix}$$

x - unitless parameter

Determine the change of the lattice parameters due to such a strain:

$$\begin{pmatrix} \mathbf{a}'_1 \\ \mathbf{a}'_2 \\ \mathbf{a}'_3 \end{pmatrix} = \begin{pmatrix} \mathbf{a}_1 \\ \mathbf{a}_2 \\ \mathbf{a}_3 \end{pmatrix} \left(\hat{I} + \hat{\varepsilon} \right) = \dots$$

Change of the total energy due to such a strain:

$$\Delta E(x) = \Delta E(-x) = \frac{1}{2} V_0 C_{44} x^2$$

Make a fit with this function.

POINT [A]

Use the [monoclinic unit cell](#) in order to model such a strain:

```
ibrav = 12
celldm(1) = |a'_1|
celldm(2) = |a'_2|/|a'_1|
celldm(3) = |a'_3|/|a'_1|
celldm(4) = a'_1 · a'_2 / (|a'_1||a'_2|)
```

POINT [B]

As before, use `ibrav = 0` and compare the results.

Relax your structure for every value of x , in order to find the minimum of energy!